## **ICRF Heating Using Antennas with Controlled Wave-number on LHD**

LHDにおける波数制御アンテナによるICRF加熱

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The large helical device (LHD) has fifteen experiment cycles so far. The ion cyclotron range of frequencies (ICRF) heating has been carried out successfully on LHD. A long pulse plasma discharge up to about one hour (54 minutes) has been achieved using the poloidal array (PA) antennas. In the  $14^{th}$  experiment cycle (2010) the toroidal array (TA) antenna was newly installed. This TA antenna consists of two antennas arrayed in the toroidal direction and has a controllability of the wave number along the magnetic field line. In the  $15^{th}$  experimental cycle (2011) the plasma with high density up to  $3.6 \times 10^{19} \text{m}^{-3}$  was sustained with 2MW of the injected RF power using both PA and TA antennas. In this experimental cycle the optimized plasma heating condition was precisely examined against the minority hydrogen ratio in the wide range of the plasma density. In addition the long pulse plasma discharge in the higher density with the higher RF power was achieved.

### **1. Introduction**

The large helical device (LHD) has fifteen experiment cycles so far. Many experiment results have been achieved, i.e., the high performance plasmas with the high density, the high beta, and the high ion and electron temperature. An ion cyclotron range of frequencies (ICRF) heating has been carried out successfully: High RF power heating up to 1.5MW and the long pulse plasma discharge up to about one hour (54 minutes) have been achieved using the poloidal array (PA) antennas [1-2]. In the 14<sup>th</sup> experiment cycle (2010) the toroidal array (TA) antenna was installed [3]. This newly installed TA antenna consists of two antennas arrayed in the toroidal direction. In the 15<sup>th</sup> experimental cycle (2011) the poloidal array (PA) antenna was installed again.

### 2. ICRF heating antennas

The TA antenna has a controllability of the wave number along the magnetic field line  $k_{//}$  with changing the phase difference between them. When two TA antennas are seen from the plasma axis, they look like to handshake each other and so they are called as HAS (<u>Handshake</u>) antenna. In the 15<sup>th</sup> cycle another pair of the poloidal array (PA) antennas was installed again. Therefore the ICRF heating experiment was carried out using four antennas.

An RF power with frequency of 38.5MHz was supplied to each antenna from the each RF generator, which consists of three stage amplifiers, i.e., 5kW, 100kW and 1MW of the RF power level in each amplifier. An impedance matching system with the liquid stub tuners was employed to reduce the reflected RF power from the ICRF heating antenna. A real-time impedance matching was capable with changing the liquid height during the ICRF heating.

A minority heating method for the ICRF heating was employed: The minority ion was a hydrogen ion with the He ion as the majority. The magnetic field strength on the plasma axis, i.e.,  $R_{ax}$ =3.6m was employed as B=2.75T.

### **3. Experimental results**

### 3-1. Plasma discharge with higher density

The plasma was sustained with ICRF heating power up to 0.5~2MW and sometimes with the assist of ECH power up to 0.2~0.6MW. First the trial of achieving the higher density plasma was carried out. In general the maximized density was almost proportional to the injected RF power. The plasma collapse occurred when the radiated power exceeds to about 40% of the absorbed RF power to the plasma. The highest density plasma with  $n_e=3.6 \times 10^{19} \text{m}^{-3}$  was sustained for 10 seconds with the ICRF heating power of 2.0MW and the ECH power of 0.37MW. Then the plasma stored-energy (W<sub>p</sub>) attained to 300kJ.

### 3-2. Plasma stored energy with ICRF heating

In the series of the plasma sustained only with the ICRF heating and the ECH power, the wide range of the plasma density,  $n_e=0.6\sim3.6\times10^{19}m^{-3}$ were obtained with the injected heating RF power  $P_{RF}$  up to 2.35MW. The plasma stored-energy  $W_p$ was increased with the density  $n_e$  and  $P_{RF}$  in the following equation of the ISS04 scaling [4];

$$W_p \propto n_e^{0.54} P_{RF}^{0.3}$$

These data are plotted in the plain of  $W_p/P_{RF}^{0.39}$  vs.  $n_e$ . The envelope of data points has a scaling of  $n_e^{0.54}$ , but many data were found below the envelope in the higher (>  $2.5 \times 10^{19} m^{-3}$ ) and the lower (<  $1 \times 10^{19} m^{-3}$ ) density. It was thought the smaller  $W_p$  was caused with the non-optimized ratio of the minority hydrogen ion as described later.

# **3-3. ICRF heating efficiency and coefficient of ISS04**

It was thought that the ICRF heating efficiency should have been a key parameter to determine the attained  $W_p$ . It mainly depends on the minority hydrogen ion ratio to the bulk helium ion. Employing ISS04 the ICRF heating efficiency  $\eta$  was derived as follows;

$$\eta \propto W_p^{2.56} n_e^{-1.38} P_{RF}^{-1}$$

In the wide range of  $n_e$  (0.6~3.8x10<sup>19</sup>m<sup>-3</sup>),  $W_p$  (70kJ~300kJ) and  $P_{RF}$ (0.5MW~2.35MW),  $\eta$  were plotted against H/(H+He). Here the intensity ratio of the visible H $\alpha$  to that of HeI at the periphery of the plasma [5] was employed to evaluate the  $\eta$  in place of minority hydrogen ion ratio. The calculated  $\eta$  was an arbitral unit, but it increased from 1.0~2.5 with H/(H+He), i.e., 10~30%. On the other hand the  $\eta_{RF}$  was deduced with the break-in slope of  $W_p$  and the RF power modulation method. However the dependence of  $\eta_{RF}$  on H/(H+He) was opposite to that of  $\eta$ .

Then it was proposed that the ISS04 scaling might have another coefficient, referred to as  $C_{eff}$ , which depended on H/(H+He) in the ICRF heating. These data were plotted again against H/(H+He) in accordance with

$$C_{eff} \eta_{RF}^{0.39} \propto W_p n_e^{-0.54} P_{RF}^{-0.3}$$

The  $C_{\text{eff}}$  indicates how the plasma heating method depends on the energy confinement time. The minority ion heating was employed in this ICRF heating scenario. First the high-energy minority hydrogen ion is produced with the RF electric field.

This energy is transferred to the bulk electron and bulk helium ion. This power fraction depends on the relation between the energy distribution of the minority hydrogen ion and the electron temperature. When the density of the minority hydrogen ion  $n_H$  is increased, i.e., the larger H/(H+He), the tail hydrogen ion temperature decreases with  $n_H$ , and the power from the hydrogen ion with the high-energy flows mainly to the bulk helium ion. It was thought that the above  $C_{eff}$  was improved with the increase in the heating power flow to the bulk ions.

### 3-4. Fueling hydrogen to ICRF heated plasma

Three methods were succeeded in fueling hydrogen to the RF plasma; one was a conventional puffing of the mixed helium gas with hydrogen gas, and the second and the third were the hydrogen pellet injection and the super sonic hydrogen injection with the repetition rate of a few Hz.

### 3-5. Long pulse plasma discharge

A long pulse plasma discharge was carried out using only RF power, e.i., ICRF heating power and ECH power. The plasma of  $n_e=2x10^{19}m^{-3}$  and  $W_p=170kJ$  was sustained for 93 seconds with  $P_{ICH}=1.6MW$  and  $P_{ECH}=0.6MW$ . The plasma of  $n_e=1.4x10^{19}m^{-3}$  and  $W_p=130kJ$  was sustained for 320 seconds with  $P_{ICH}=0.8MW$  and  $P_{ECH}=0.3MW$ .

### Summary

The ICRF heating was carried out using the new TA antenna and the PA antenna. The higher density of  $3.6 \times 10^{19} \text{m}^{-3}$  was sustained for 10 seconds with P<sub>ICH</sub>=2MW and P<sub>ECH</sub>=0.37MW. The higher plasma stored-energy was found at ~20% of H/(H+He). In this range of H/(H+He) the ICRF heating efficiency was degraded, but the coefficient of the energy confinement was much improved in ~20% of H/(H+He). The duration time of the long pulse discharge was extended in the higher density with the higher RF heating power.

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