## Regression Approach for Acquiring a Quantitative Guidance toward Updating the Deuterium-Deuterium Fusion Neutron Emission Rate in the Large Helical Device

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A regression approach has been adopted to acquire a quantitative guidance for updating the total neutron emission rate ( $S_n$ ) in the Large Helical Device (LHD) with employing the externally controllable parameters such as heating power and plasma density. A deduced regression expression is worthwhile to understand for the contribution of an individual parameter during high  $S_n$  discharges, and then to be exploited in the experiment planning to update the record  $S_n$  value in LHD in the coming campaigns. It was found that  $S_n$  in high  $S_n$  discharges in LHD is expressed as  $S_n = 10^{14.25} \times n_{e_avg}^{0.52} \times P_{N-NB}^{0.69} \times P_{P-NB}^{0.37}$ , where  $n_{e_avg}$ ,  $P_{N-NB}$ , and  $P_{P-NB}$  represent the line-averaged electron density  $[10^{19} \text{ m}^{-3}]$  and the injection power of negative and positive ions based neutral beam injection [MW], respectively. This expression shows that, among three parameters,  $P_{N-NB}$  is essential for achieving high  $S_n$  in this employed high  $S_n$  discharge database.

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In deuterium-tritium (DT) fusion burning plasmas, the energy of DT fusion neutron absorbed by the blanket module is used for generating electrical power. Therefore, the fusion output from the plasma is the direct measure to show the accomplishment for realizing a fusion reactor. In a deuterium-deuterium (DD) experiment performed in large tokamaks e.g. TFTR, JT-60U, and JET, the total neutron emission rate (S<sub>n</sub>) achieved approximately  $5 \times 10^{16}$  n/s which corresponds to the fusion output of approximately 60 kW [1–3]. In JET, empirical formulas of  $S_n$  were deduced for a prediction of the counting rate of the neutron camera [4]. The fusion performance of large-scale helical device has been indicated after starting deuterium operation in the Large Helical Device (LHD) in 2017. DD fusion performance, e.g.  $S_n$  of  $\sim 3.3 \times 10^{15}$  n/s and  $\sim 3.0 \times 10^{15}$  n/s were achieved in deuterium pellet and gas puff discharges, simultaneously using intensive neutral beam (NB) injections [5,6]. In these high  $S_n$  discharges, simultaneous precise adjustments of experimental conditions such as a magnetic configuration, heating pattern, and density control are required, because in NB heated LHD plasmas, S<sub>n</sub> depends on the plasma parameters such as plasma temperature and density as well as the injection energy and power of NBs. For updating S<sub>n</sub> record in LHD, grasping the importance of each externally controllable parameter helps to decide the priority of adjustment of experimental conditions. In addition, this regression approach may contribute to controlling the steady state fusion reactor in the future. This paper represents the first result of an application of the regression approach for  $S_n$  in LHD. It is noted the here the same approach has been conducted to deduce regression expression of thermal diffusivities in high ion temperature plasmas in LHD with simple and plausible results [7].

We performed the experiment in NB heated deuterium plasmas using electron cyclotron heating (ECH), negative ion based neutral beam (N-NB) injections whose injection energy is up to 180 keV, and positive ion based neutral beam (P-NB) injections whose injection energy is up to 60/80 keV. The experimental data points sampled for this study satisfy the following general restrictions. (1). The preset magnetic axis position is 3.55 m, toroidal magnetic field strength is 2.89 T, the direction of the toroidal magnetic field is counterclockwise when viewed from above because this is the typical magnetic configuration of the high  $S_n$  discharge. (2). Line-averaged electron density  $(n_{e_{avg}})$  is 1-3 × 10<sup>19</sup> m<sup>-3</sup>. (3). The working gas is deuterium. (4). The working gas of N-NB and P-NB is deuterium and both N-NB and P-NB are injected without breakdown or sudden (or unintended) stop. (5). The intensity ratio of  $D\alpha$  to  $H\alpha$  is more than nine to one, which implies deuterium-dominant plasmas. (6). The timing is not an initiation phase of the discharge to avoid timing before NB absorption. Figure 1 shows the typical time evolution of NB heated deuterium plasma discharge. The region colored in yellow corresponds to the region of interest in



Fig. 1 Typical time evolution of deuterium plasma discharge. Yellow region fulfills the general restrictions in this analysis.

this database. The injection power of N-NB ( $P_{\text{N-NB}}$ ), P-NB ( $P_{\text{P-NB}}$ ), and ECH ( $P_{\text{ECH}}$ ) is ~6 MW, up to 18 MW, and 2.5 MW, respectively. The  $n_{\text{e_avg}}$  measured by the interferometer shows only a gradual change. The central electron temperature ( $T_{e0}$ ) measured by the Thomson scattering diagnostics shows  $T_{e0} \sim 3 \text{ keV}$ . The  $S_n$  measured by the neutron flux monitor [8] gradually increases, depending on the heating power. For each discharge, the database contains measured data value of up to 10 points. The number of available discharges is 443, with summing up the total of 1590 data points.

To identify the importance of parameters for  $S_n$ , only externally controllable parameters are used to conveniently plan the experimental scenario. Those parameters are  $n_{e_avg}$  [10<sup>19</sup> m<sup>-3</sup>],  $P_{N-NB}$  [MW],  $P_{P-NB}$  [MW], and  $P_{ECH}$ . During regression analysis, it was found that the importance of  $P_{ECH}$  is relatively low compared to the other parameters. The so-called log-linear multivariate regression is conducted to obtain the regression expression as

$$S_{\rm n} = 10^{14.25} \times n_{\rm e_{avg}}^{0.52} \times P_{\rm N-NB}^{0.69} \times P_{\rm P-NB}^{0.37}$$

The obtained expression shows that  $P_{\text{N-NB}}$  contributes the most to an increase in  $S_n$  with the largest exponent. Note that ratio of  $S_n$  in experiment to regression prediction in highest  $S_n$  case is 1.13.

Figure 2 shows the comparison of  $\log_{10}S_n$  values between the experimental measurement and ones based on the regression expression. Although the coefficient of determination,  $R^2$ , is as relatively high as 0.84, there are groups of data points (mostly data with  $S_n$  less than 10<sup>15</sup>) deviating largely from the diagonal line shown in Fig. 2. In this study, we simply tried to express  $S_n$  using only a





Fig. 2 Comparison of  $\log_{10} S_n$  values between the experimental measurement (vertical axis) and ones based on the regression expression (horizontal axis).

limited number of parameters which are externally controllable in terms of experimental planning. The regression can be improved if we employ the measurable plasma parameters such as temperature and density profiles such as described in Ref. [7]. This extended study will be performed in our future work. It is also noted that the regression expression is only valid in the range of an employed database. However, it would be worthwhile to extend the parameter regime of  $S_n$  gradually beyond it, that is, targeting record  $S_n$  value.

The regression analysis of  $S_n$  in deuterium LHD plasma was initiated to identify the importance of each externally controllable parameter for achieving higher  $S_n$ . The obtained expression shows that the injection power of N-NB is relatively important compared with the plasma density and injection power of P-NB in high  $S_n$  discharge database. The experiment targeting updating  $S_n$  record will be performed in coming LHD campaigns, based on this quantitative guidance deduced in this study.

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