# Strategy for the Development of Tokamak DEMO Reactor with Hybrid Scenario

ハイブリドシナリオを用いたトカマク原型炉開発戦略

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A tokamak DEMO concept using the hybrid scenario (HbS) is proposed. The HbS is quite convenient for the DEMO development with high reliability and high flexibility. A high aspect-ratio line would be desirable for the safety and HbS. An example of HbS DEMO with major radius  $R_0 \sim 9$  m and  $Q = 20 \sim 30$  is shown, where the long pulse length of 4~10 hours is achievable for the moderate bootstrap current fraction  $f_{BS} = 0.5 \sim 0.6$ , current drive efficiency  $\gamma_{CD} = 0.3 \sim 0.4$  and ohmic current fraction  $f_{OH} = 0.1 \sim 0.3$ .

## 1. Introduction

After the Fukushima nuclear disaster March 2011, the R&D policy for nuclear fusion DEMO reactors has been reconsidered in Japan [1]. In order to reduce the neutron load and heat load for the plant safety, the net electric power  $P_{\text{net}}$  could be lowered to several hundred MWe routinely from the previous value of  $P_{\text{net}} \sim 1 \text{ GWe}$  (; fusion output power  $P_{\text{F}} \sim 3 \text{ GW}$ ).

A steady-state tokamak reactor (SSTR) with the efficient utilization of the boot-strap current was proposed [2]. To generate  $P_{\rm F} = 2.5 \text{ GW}$ , the major radius of SSTR was designed as  $R_0 = 9$  m. Afterwards to pursue the economy of construction cost, a compact tokamak reactor concept with sliming the central solenoid coil (SlimCS) was set forth, where  $R_0$  was decreased to 5.5 m maintaining  $P_{\rm F} = 3$  GW [3]. On the other hand, the pulse tokamak reactor concept has survived. An inductive-drive long-pulse tokamak (IDLT) with  $P_{\text{net}} = 1 \text{ GWe had } R_0 = 10 \text{ m } [4].$  The neutron wall load in these reactors was  $\Gamma_{\rm n} \sim 3 \text{ MW/m}^2$ , and could bring about the wall melt due to the uncontrollable decay heat under the severe accident. Recently a renewal DEMO conceptual design was proposed, where  $P_{\text{net}} \approx 800 \text{ MWe}$  and  $\Gamma_n \approx 1 \text{ MW/m}^2$  with  $R_0 \approx$ 8 m [5]. The equipped CS coil is able to supply the magnetic flux required for the current ramp-up. On the other hand in EU for a long time, there have been a strategy of the pulsed operation to accelerate a DEMO program [6].

The present report proposed a tokamak DEMO concept using the hybrid scenario (HbS), which is planned for ITER to test the various engineering components towards DEMO with high reliability, high neutron fluence and long pulse length [6,7]. The fraction of the non-inductive current,  $f_{\rm NI}$ , including the bootstrap current is expected to be 40~60% in the ITER HbS, and to be larger than 70% in the DEMO HbS. The CS coil supplies the

magnetic flux for the ohmic current over several hours. The HbS will enhance the operational flexibility of the DEMO reactor to realize finally the nuclear fusion commercial reactor, whichever steady-state reactor or long-pulse reactor.

# **2.** Requirement of Confinement Performance and Current Drive Power

The tokamak reactor should have a certain plasma current  $I_p$  for high Q (fusion gain) operation to generate the net electric power output. The minimum condition  $H_H I_p A > 50$  MA was given in Ref. [6], where  $H_H$  is the confinement improvement factor from H98 scaling and  $A = R_0/a$  is the aspect ratio. Taking account of the fuel dilution ( $C_f = 2n_{\text{DT}}/n_e$ ), the core radiation cooling ( $C_r = 1 - P_{\text{rad}}^{\text{core}}/P_{\text{abs}}$ ), the operation density ( $N_{\text{GW}} = \pi a^2 \langle n_e \rangle/I_p$ : m<sup>2</sup>, 10<sup>20</sup>/m<sup>3</sup>, MA) and the operation-temperature effect, the condition is approximately expressed as

$$H_H I_p A > 12 \langle T \rangle^{0.56} / (C_f^2 C_f)^{1/3} (1 + 5/Q)^{1/3} F(N_{GW}) \text{ MA}$$
(1)

assuming the averaged temperature  $10 \text{ keV} < \langle T \rangle < 20 \text{ keV}$ , and the degradation factor  $F(N_{\text{GW}}) < 1$  at the high density  $N_{\text{GW}} \sim 1$ . When the fuel dilution and the core radiation are small,  $C_{\text{f}} = C_{\text{r}} = 0.85$ , the condition is  $H_H I_p A > 50 \text{ MA}$  for  $\langle T \rangle = 10 \text{ keV}$  and  $H_H I_p A > 75 \text{ MA}$  for  $\langle T \rangle = 20 \text{ keV}$ . Design parameters in Ref. [5],  $I_p \approx 14 \text{ MA}$ ,  $A \approx 3.4 (R_0 = 8.2 \text{ m}, a = 2.4 \text{ m}, \kappa = 1.85)$ ,  $\langle T \rangle \approx 20 \text{ keV}$ ,  $Q \approx 20$ ,  $H_H \approx 1.5$  and  $N_{\text{GW}} = 0.82$ , satisfy this condition.

The fusion output power is estimated as

$$P_{\rm F} \approx 0.07 \left( \kappa/R_0 \right) \left( C_{\rm f} N_{\rm GW}/H_H \right)^2 \left( H_H I_{\rm p} A \right)^2 \left\langle T \right\rangle^{1.5} \, \rm MW \ (2)$$

The design value of  $P_{\rm F} = 1400$  MW in Ref. [5] agrees with this estimation. Under the condition (1), both  $P_{\rm F}$  and  $\Gamma_{\rm n}$  are decreased with the increase of A by fixing a,  $N_{\rm GW}$  and  $\langle T \rangle$ ;  $P_{\rm F} \sim 1/A$  and  $\Gamma_{\rm n} \sim 1/A^2$ . If we increase  $H_H I_p A \sim A^k$  and  $\langle T \rangle \sim A^{1.8k}$  by fixing *a* and  $N_{\text{GW}}$ , we can choose  $P_F \sim A^0$  and  $\Gamma_n \sim 1/A$  with k = 1/4.7 or  $P_F \sim A$  and  $\Gamma_n \sim A^0$  with k = 2/4.7. From the viewpoint of safety (low  $\Gamma_n$ ), a high aspect-ratio line would be desirable.

The boot-strap current fraction  $f_{\rm BS} \sim \beta_{\rm p}/A^{1/2}$  is approximately given by

$$f_{\rm BS} \approx 0.5 (A/3.4)^{1/2} (H_H N_{\rm GW} \langle T \rangle / 15) (50/H_H I_p A)$$
 (3)

where we refer to an ITER steady-state operation parameter;  $f_{BS} = 0.5$  at A = 3.4,  $H_H = 1.6$ ,  $N_{GW} = 0.8$ ,  $\langle T \rangle = 12$  keV and  $I_p = 9$  MA. When  $H_H I_p A = 50 \sim 75$ MA and  $\langle T \rangle = 10 \sim 20$  keV, the  $f_{BS}$  value is (0.33~0.44)  $\times H_H N_{GW}$ . It is difficult to achieve  $f_{BS} > 0.6$  within a realistic HH factor < 1.3.

The current drive power for the HbS operation is

$$P_{\rm CD} = (1/\gamma_{\rm CD}) n_{20} R_0 I_{\rm p} (1 - f_{\rm BS} - f_{\rm OH}) = (1/\pi \gamma_{\rm CD} R_0) (N_{GW}/H_{\rm H}^2) (H_{\rm H} I_{\rm p} A)^2 (1 - f_{\rm BS} - f_{\rm OH}) MW$$
(4)

where the current drive efficiency  $\gamma_{CD}$  is expected to be improved up to  $\gamma_{CD} = 0.3 \sim 0.4$  even for the electron cyclotron current drive [9,10]. The *Q* value defined by  $Q = P_F/P_{CD}$  is expressed as

$$Q \approx 0.2 \gamma_{\rm CD} \left( \kappa C_{\rm f}^2 N_{GW} \right) \left\langle T \right\rangle^{1.5} / \left( 1 - f_{\rm BS} - f_{\rm OH} \right) \tag{5}$$

The *Q* value is able to exceed 25 in a DEMO reactor with  $f_{\rm BS} + f_{\rm OH} = 0.8$  at a set of practical parameters;  $\gamma_{\rm CD} = 0.3$ ,  $\kappa = 1.8$ ,  $C_{\rm f} = 0.8$ ,  $N_{\rm GW} = 0.85$  and  $\langle T \rangle = 20$ keV. When  $f_{\rm OH} = 0$  and  $f_{\rm BS} \approx 0.5$  ( $H_H \approx 1.3$ ), the *Q* value will decrease to ~10 and it will become difficult to generate the net electric output power. To obtain *Q* > 25 without ohmic current contribution, a considerably high performance is required;  $f_{\rm BS} > 0.65$  ( $H_H > 1.5$ ),  $\gamma_{\rm CD} > 0.4$ ,  $\kappa = 1.8$ ,  $C_{\rm f} = 0.8$ ,  $N_{\rm GW} = 1$  and  $\langle T \rangle = 20$  keV.

In the early phase of DEMO development (conceptual design, engineering design, construction, test operation, initial operation), it is impossible to accurately know the values of  $C_{\rm f}$ ,  $C_{\rm r}$ ,  $H_H$ ,  $\langle T \rangle$ ,  $\gamma_{\rm CD}$ , and  $f_{\rm BS}$ . These values will be found through the whole DEMO operations. Further improvement of  $\gamma_{\rm CD} > 0.4$  will be expected during the DEMO construction phase and operation phase. Therefore the HbS is quite convenient for the tokamak DEMO development with high reliability and high flexibility.

### 3. Example of HbS DEMO

The radius of the CS coil is larger than 3.5 m to supply the magnetic flux  $\Phi_{CS} > 650$  V·s. During the current ramp-up, the external-inductance part  $\Phi_{ext} \sim \mu_0 R_0 I_p \sim 150$  V·s spends  $\Phi_{CS}$ , but internal-inductance and resistive parts should not consume it. The rest of  $\Phi_{HbS} \sim 500$  V·s is used for the HbS ohmic current. The plasma resistivity for  $\langle T \rangle \approx 20$  keV is lower than  $\mathcal{R}_{e} < 0.002 A$  V/MA for ( $\kappa a/Z_{eff}$ ) > 2.5 m. The possible flat-top duration is  $t_{\text{flattopt}} > \Phi_{\text{HbS}}/\mathcal{R}_{e}f_{\text{OH}}I_{p} =$  $4000/f_{\text{OH}}$  sec for  $H_{H}I_{p}A = 75$  MA. Long pulse time  $4\sim10$  hours will be achievable in a HbS DEMO with  $f_{\text{OH}} = 0.1\sim0.3$ . If the TF-coil width is  $1\sim1.5$  m, the TF-coil plasma distance is  $1.5\sim2$  m and the plasma minor radius a =  $2\sim2.5$  m, then the major radius becomes  $R_{0} \sim 9$  m. This HbS DEMO is not small, but its reliability and flexibility is high enough to realize finally the fusion commercial reactor.

#### 4. Summary

A tokamak DEMO concept using the hybrid scenario (HbS) is proposed. In the early phase of DEMO development, it is impossible to know the accurate performance. They will be found through the whole DEMO operations. The HbS is quite convenient for the DEMO development with high reliability and high flexibility. A high aspect-ratio line would be desirable for the safety and HbS. An example of HbS DEMO is shown;  $H_H I_p A \approx 75$  MA,  $\langle T \rangle \approx 20$  keV,  $H_H < 1.3$ ,  $N_{\rm GW} \approx 0.85$ ,  $f_{\rm BS} = 0.5 \sim 0.6$ ,  $\gamma_{\rm CD} = 0.3 \sim 0.4$  and  $f_{\rm OH} = 0.1 \sim 0.3$  with  $R_0 \sim 9$  m,  $Q = 20 \sim 30$  and  $t_{\rm flattop} = 4 \sim 10$  hours.

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